



3D SYSTEMS®

KU LEUVEN

# “On the influence of overheating in downfacing regions on the surface quality and geometrical accuracy”

Umberto Paggi<sup>1,2,4</sup>, Rajit Ranjan<sup>3</sup>, Lore Thijs<sup>2</sup>, Can Ayas<sup>3</sup>, Matthijs Langelaar<sup>3</sup>,  
Fred van Keulen<sup>3</sup>, Brecht van Hooreweder<sup>1,4</sup>

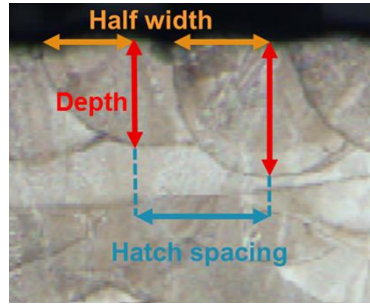
<sup>1</sup> KU Leuven, Department of Mechanical Engineering, Leuven, Belgium

<sup>2</sup> 3D Systems Leuven, Belgium

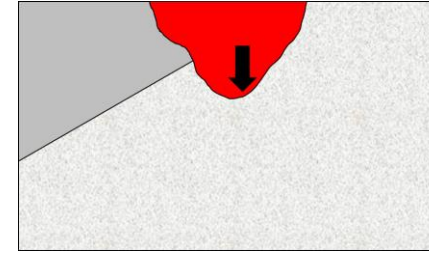
<sup>3</sup> TU Delft, Department of Precision and Microsystems Engineering (PME), Delft, the Netherlands

<sup>4</sup> Member of Flanders Make - Core lab PMA-P, KU Leuven, Leuven, Belgium

# Table of content

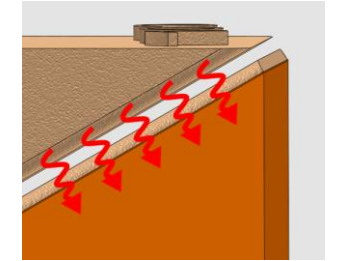
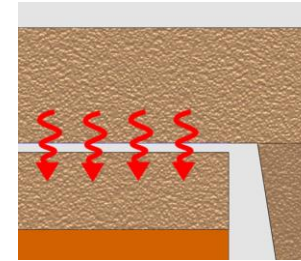
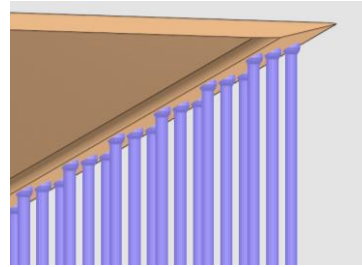


1. Melt pool and accuracy



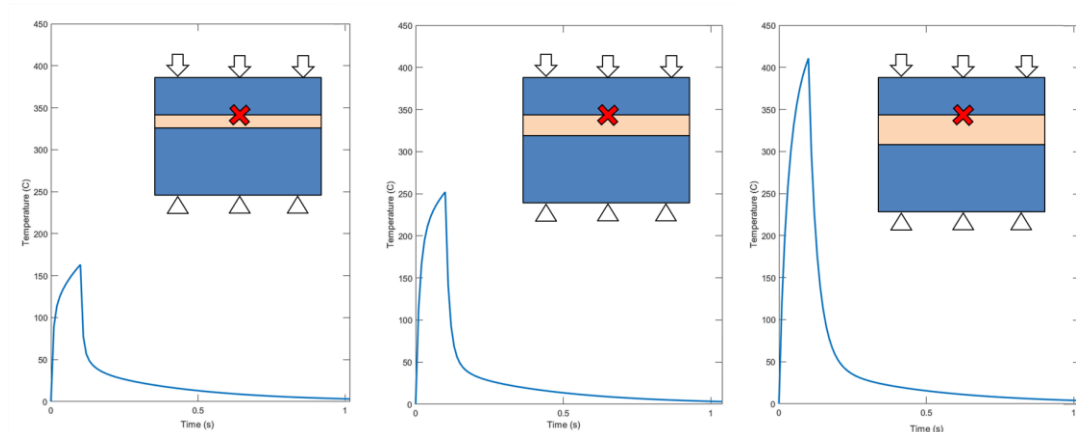
2. Overheating and fluid flow on downfacing regions

3. Improving powder bed conduction

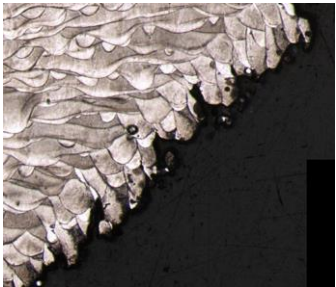
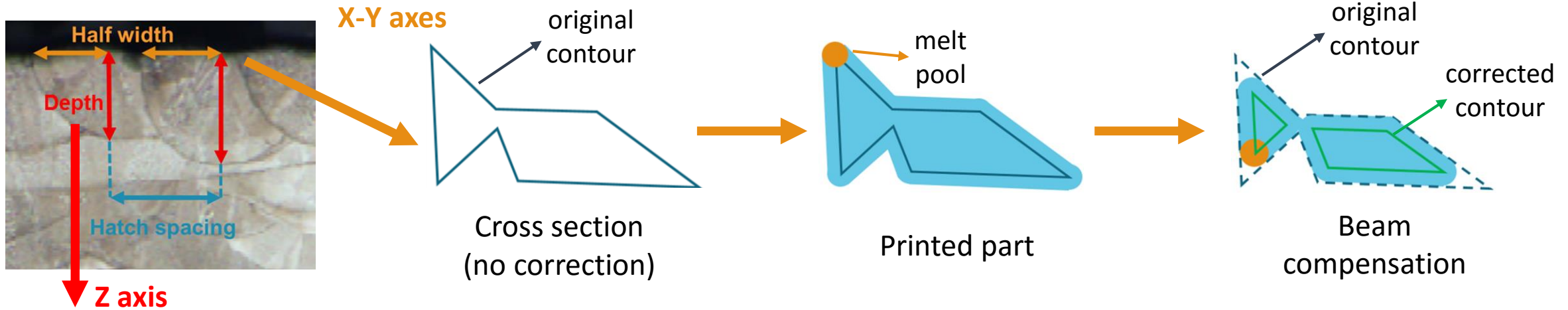


4. Understanding the gap behavior

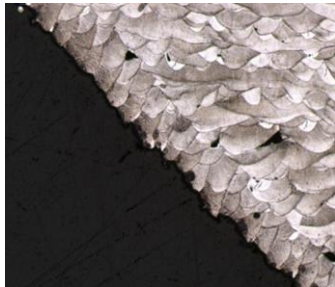
5. Thermal simulation



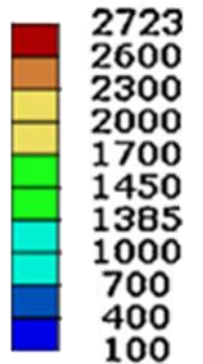
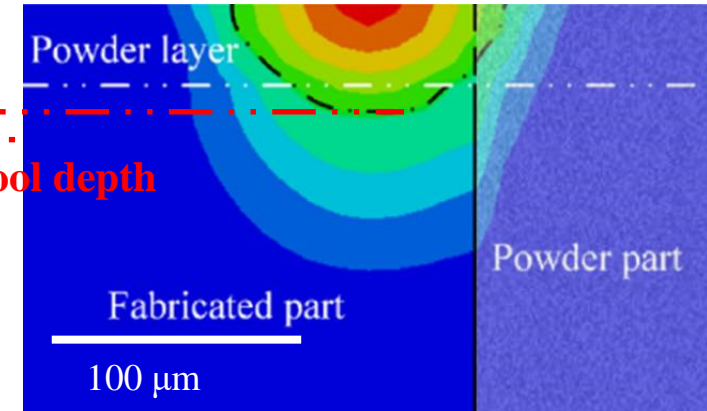
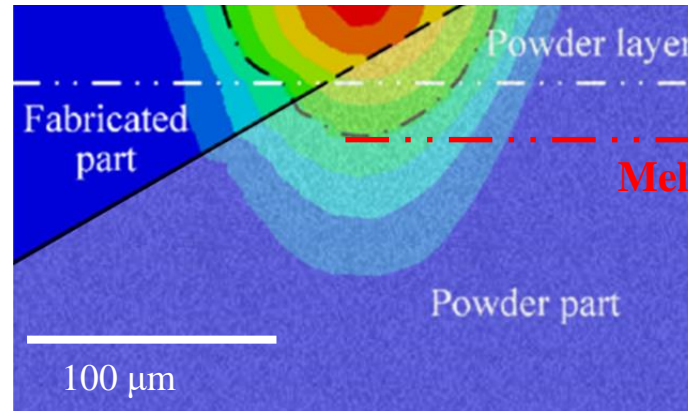
# Melt pool and accuracy



Non-optimal parameters



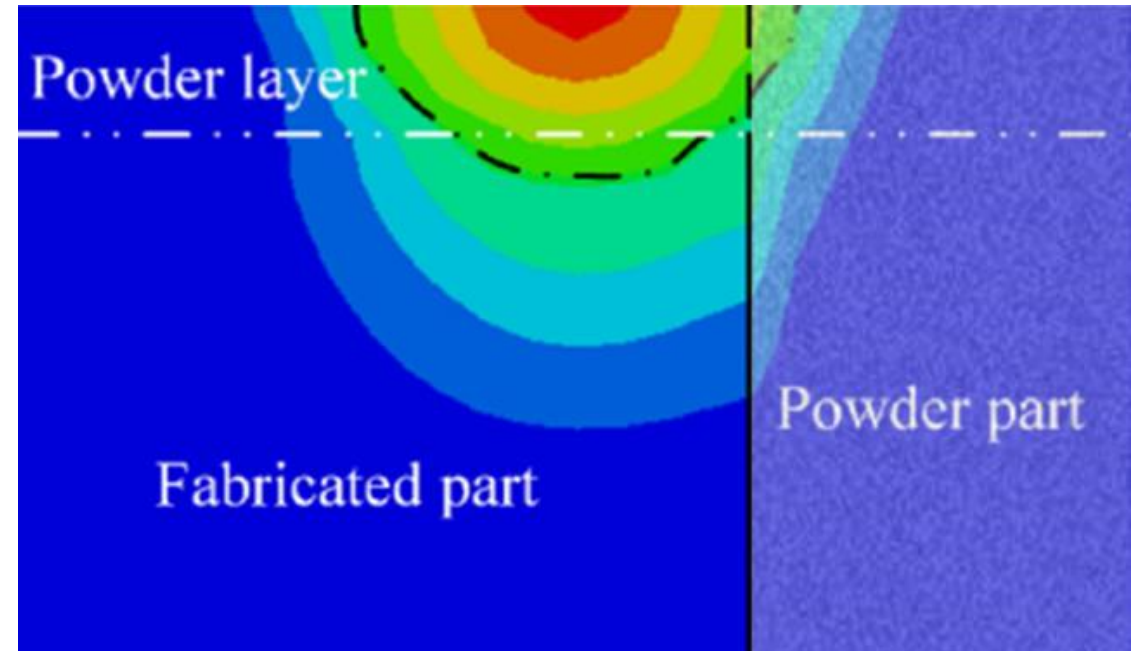
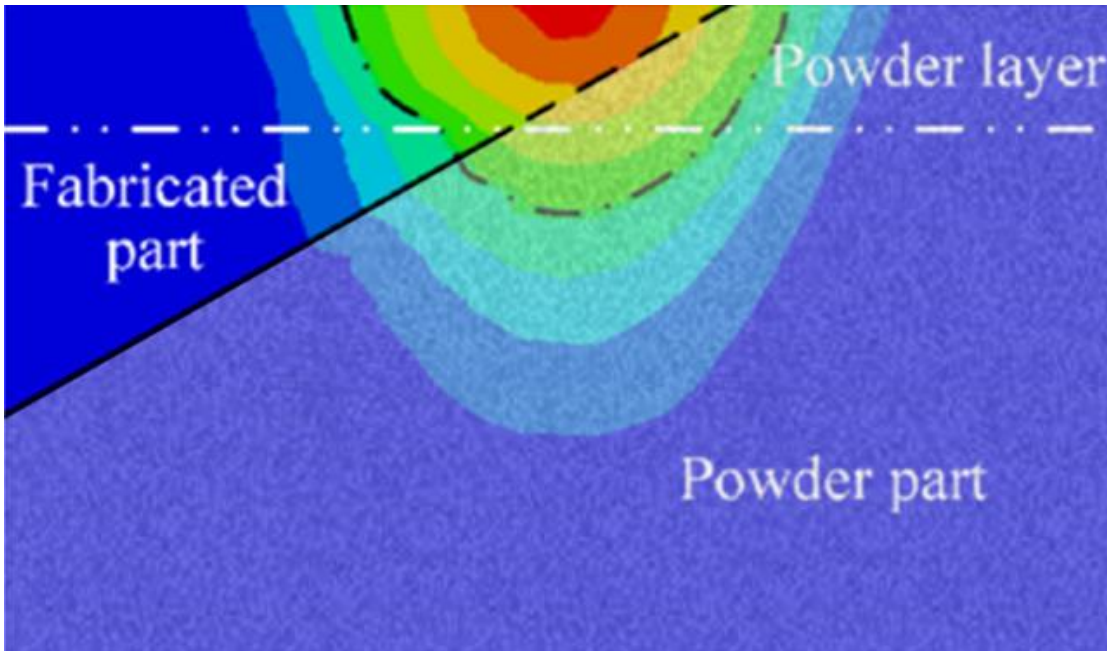
Optimal parameters



Overheating due to insulating effect of powder bed  
[Analysis of the quality of slope surface in selective laser melting process by simulation and experiments, Xiang et al., 2019]

# Overheating and fluid flow on downfacing regions

Laser scanning (overheating of the downfacing area)

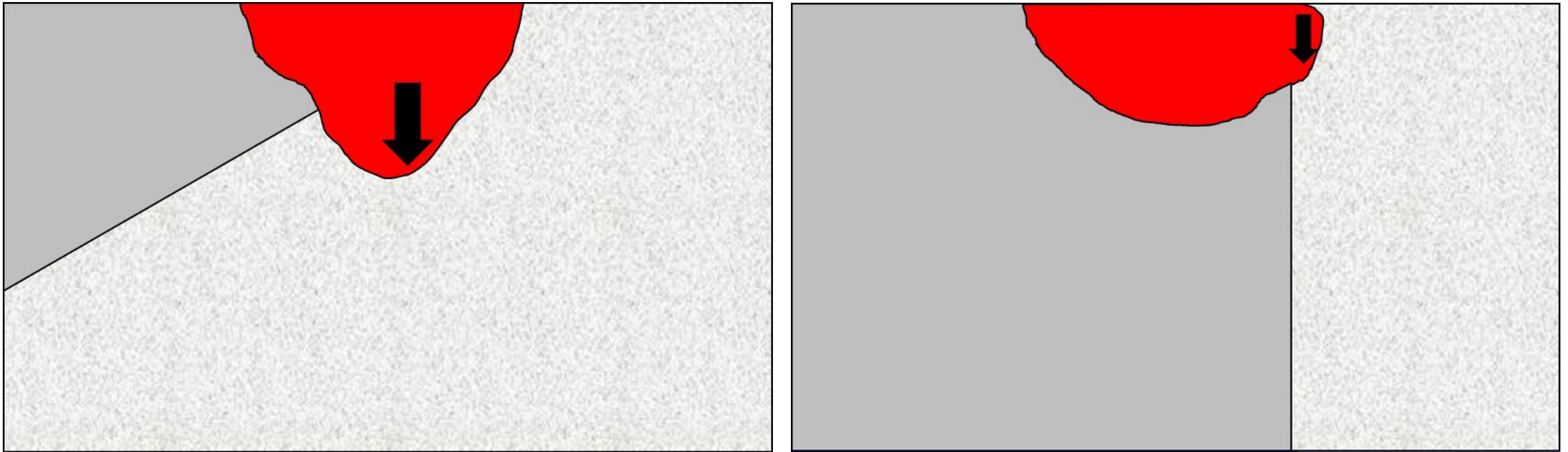




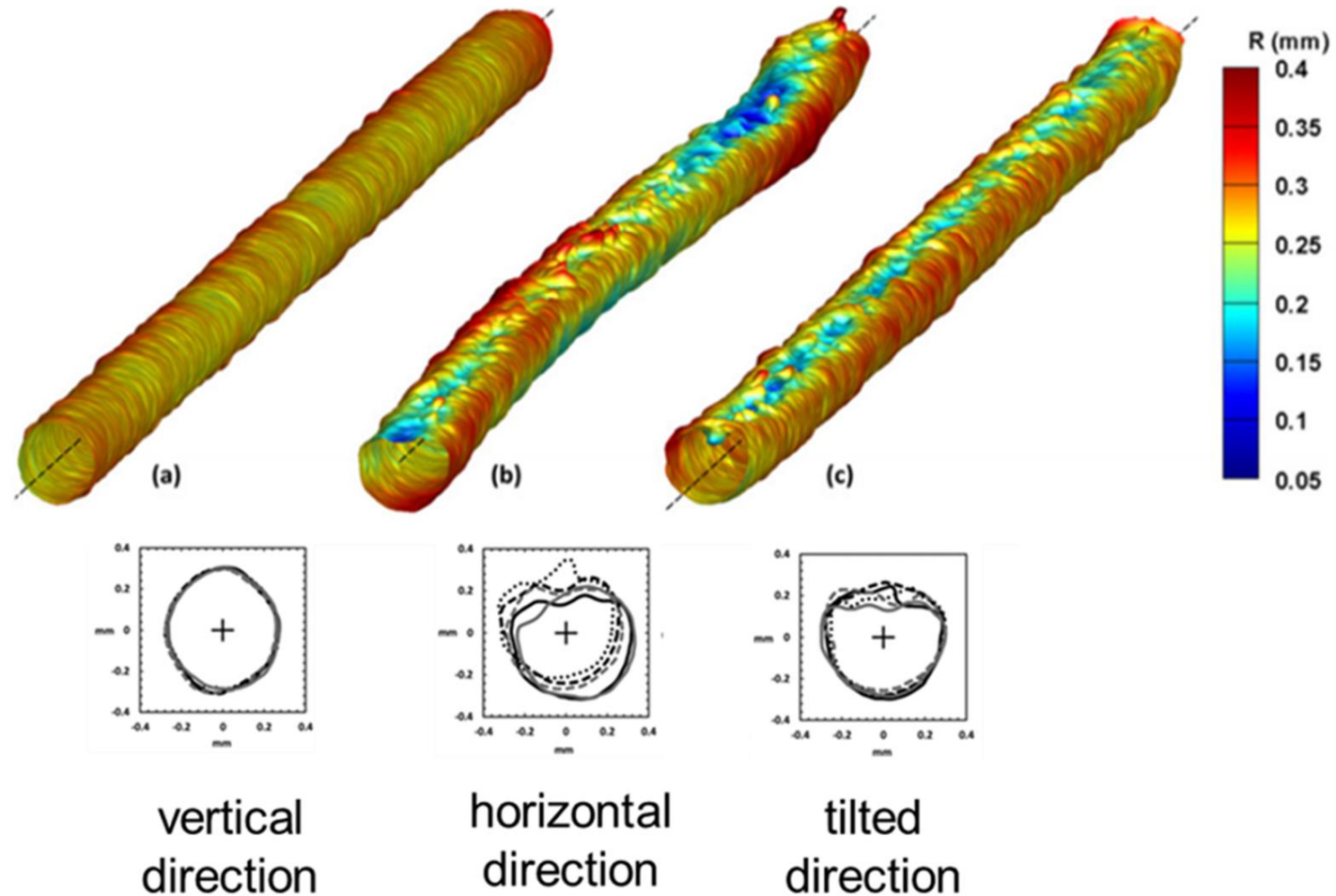
# Overheating and fluid flow on downfacing regions

Fluid flow due to gravity, recoil pressure, capillarity, turbulent flow in the melt pool...

*[Improving additive manufacturing processability of hard-to-process overhanging structure by selective laser melting, Cheng et al., 2017]*

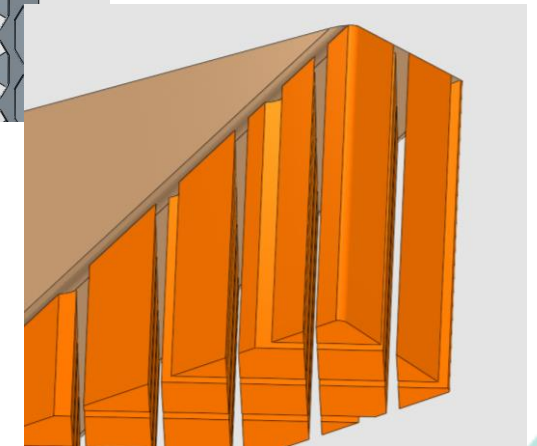
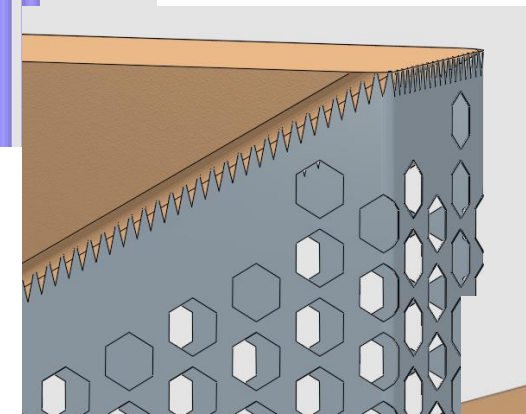
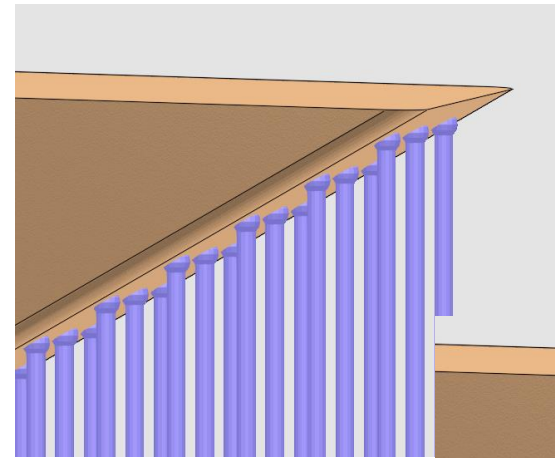
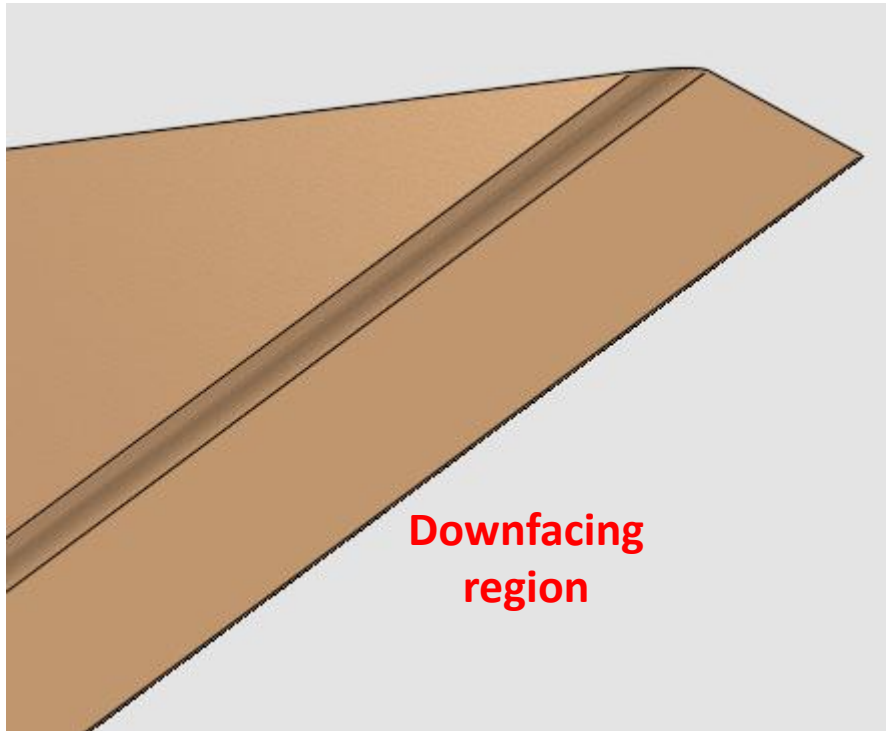


# Overheating and fluid flow on downfacing regions

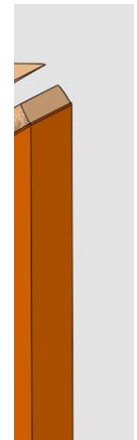
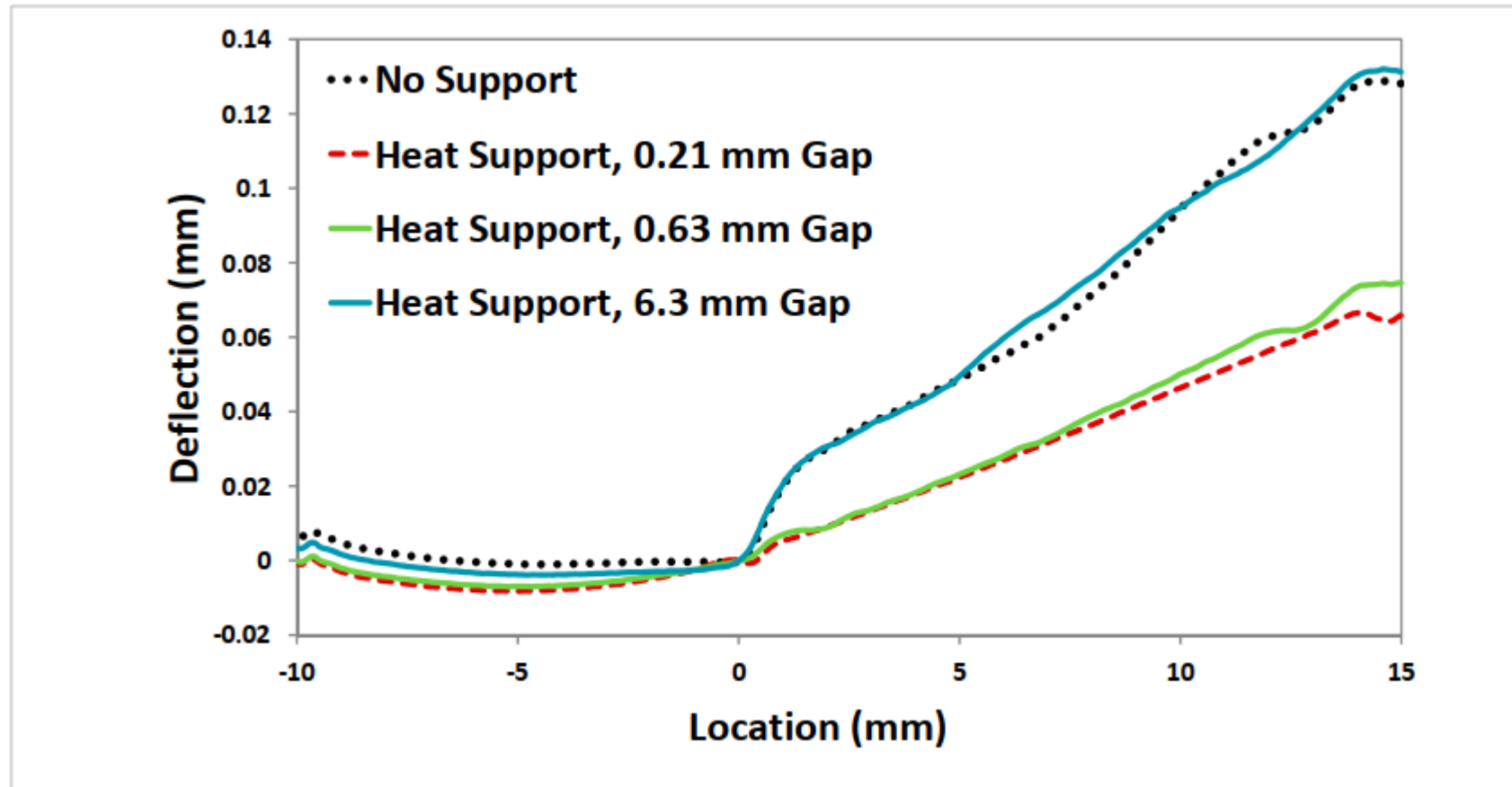


*[Build Direction Effects on Microchannel Tolerance and Surface Roughness, Jacob C. Snyder et al., 2015]*

# Improving powder bed conduction: standard support strategies



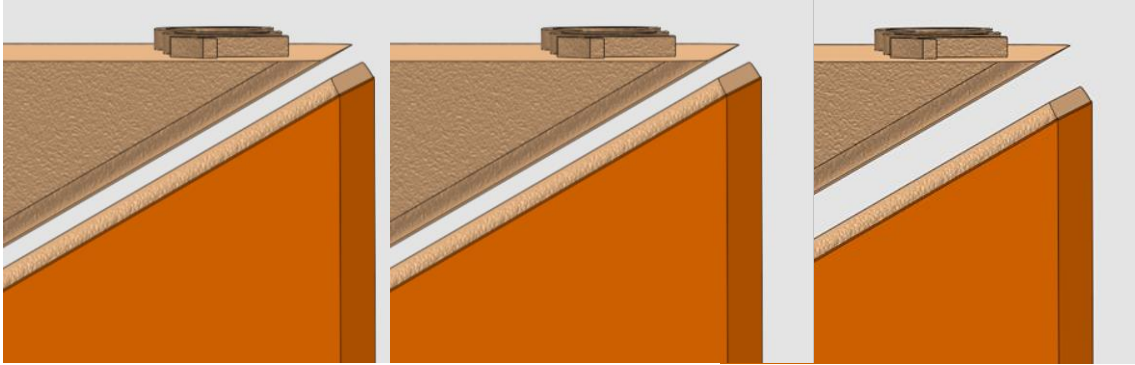
# Improving powder bed conduction: contactless thermal support



*[Contact-Free Support Structures for Part Overhangs in Powder-Bed Metal Additive Manufacturing, Cooper et al., 2017  
Deformation Evaluation of Part Overhang Configurations in Electron Beam Additive Manufacturing, Cheng and Chou, 2015]*



# Improving powder bed conduction: contactless thermal support



Gap/layer thickness = 0.5 Downfacing angle 30° Gap/layer thickness = 6



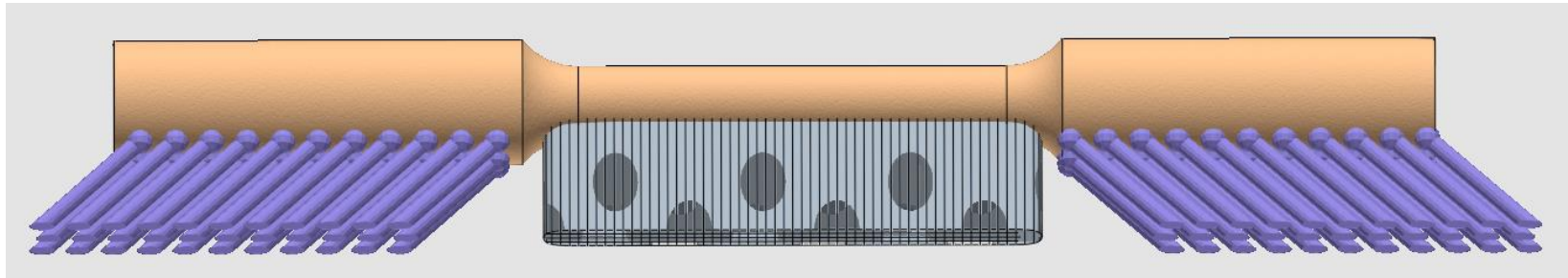
Downfacing angle 45°



ProX350 Flex

Xp 3DXpert™

# Improving powder bed conduction: standard support strategies

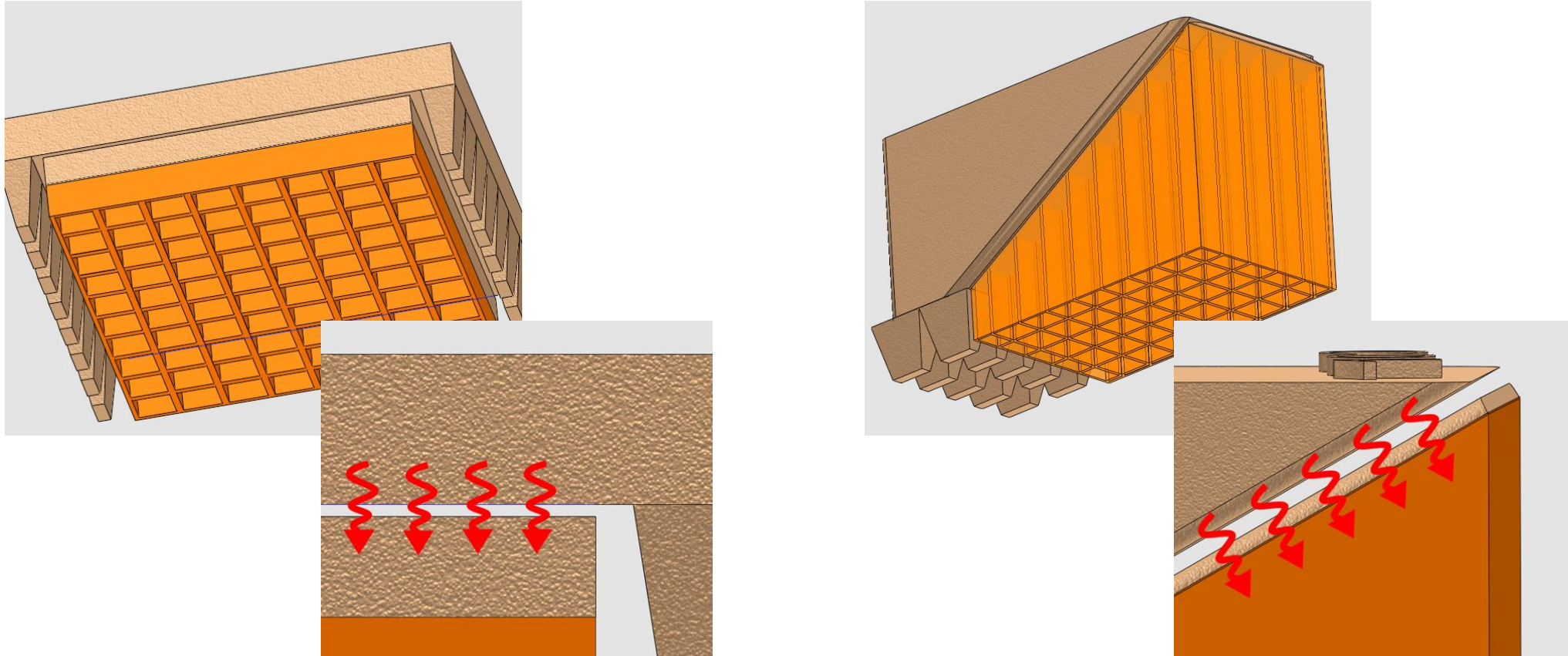


Manual support removal

Grinding

Polishing

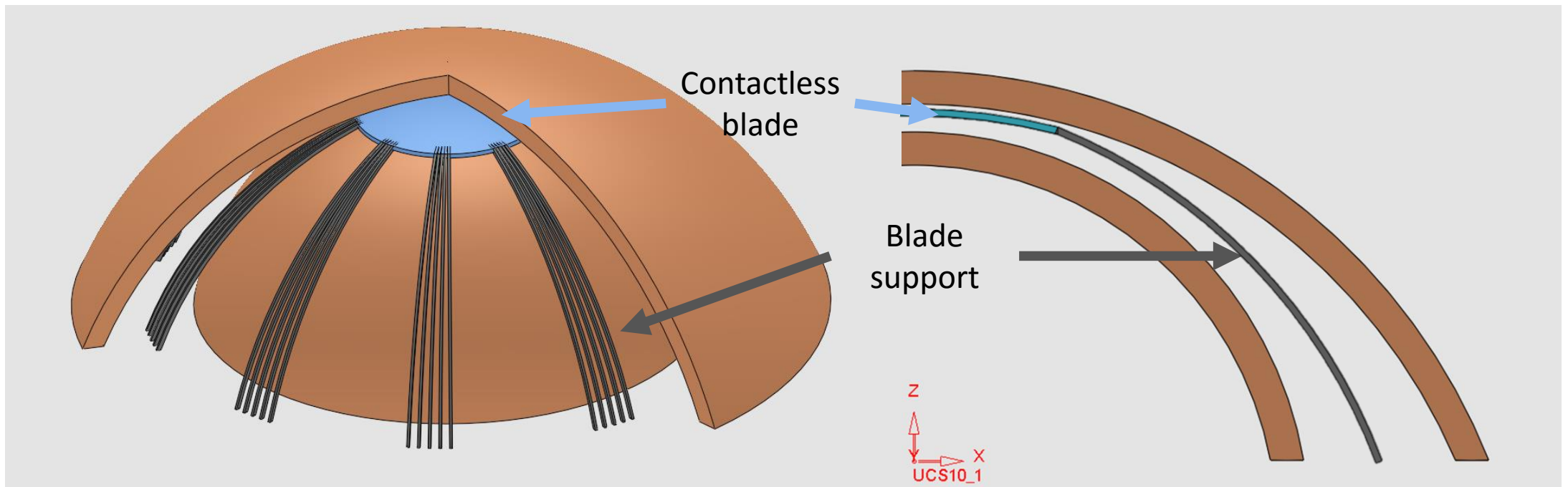
# Improving powder bed conduction: contactless thermal support



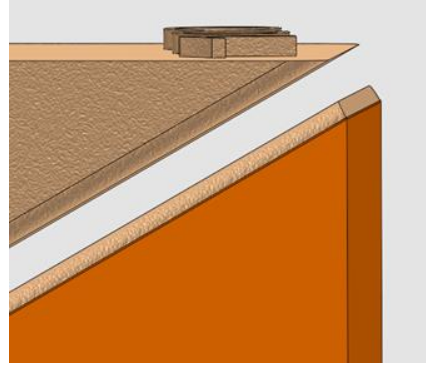
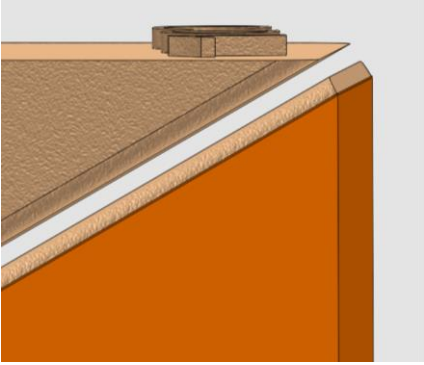
*[Contact-Free Support Structures for Part Overhangs in Powder-Bed Metal Additive Manufacturing, Cooper et al., 2017  
Deformation Evaluation of Part Overhang Configurations in Electron Beam Additive Manufacturing, Cheng and Chou, 2015]*



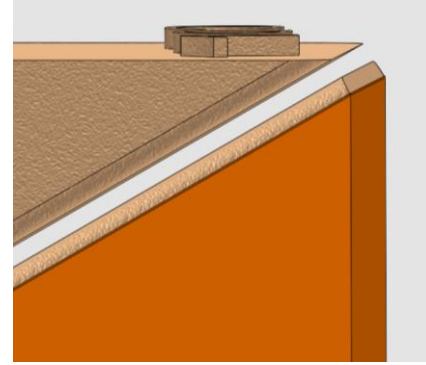
# Improving powder bed conduction: contactless thermal support



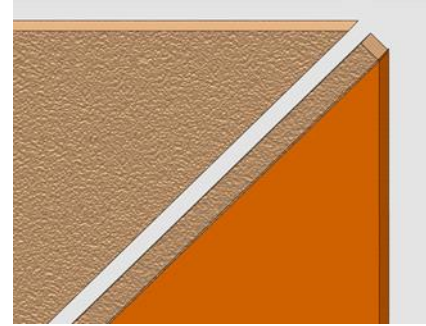
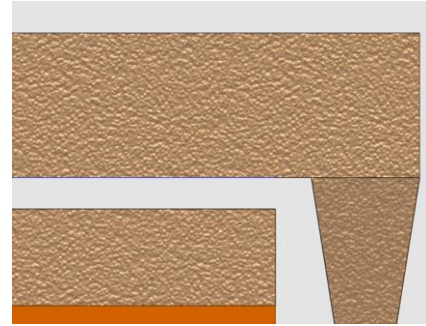
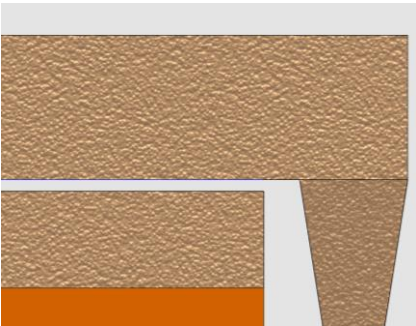
# Improving powder bed conduction: contactless thermal support



Gap/layer thickness = 0.5 → Gap/layer thickness = 6



Downfacing angle 30°



Downfacing angle 45°

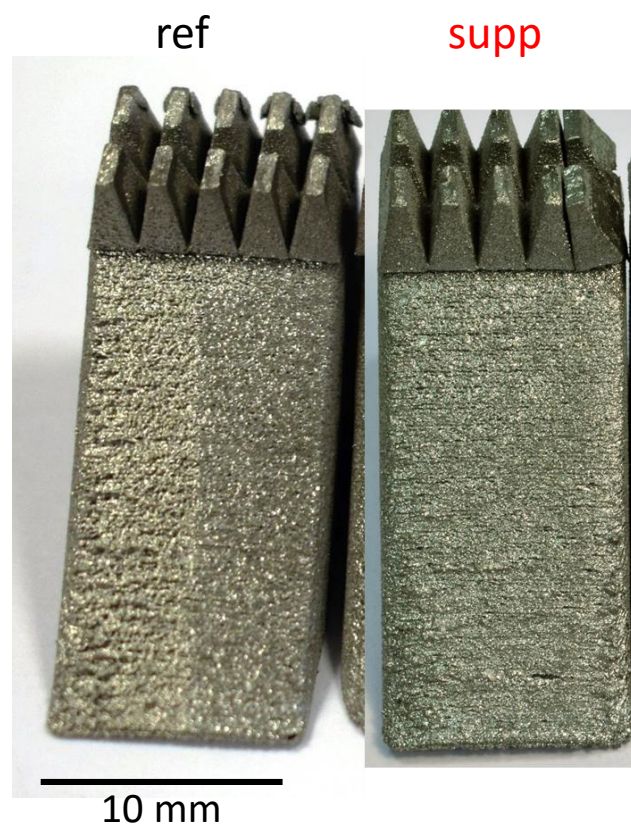


ProX350 Flex





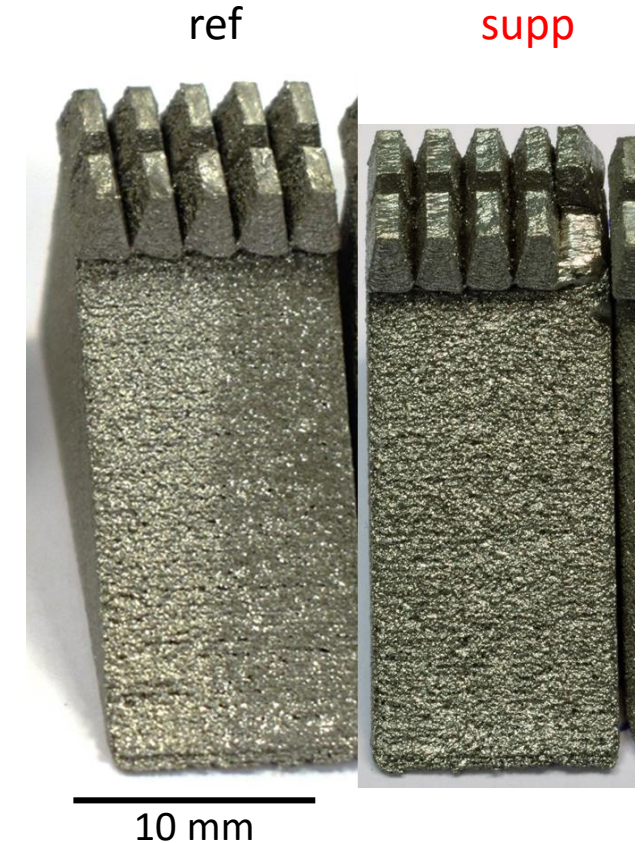
# Experimental results: 30° samples



30  $\mu\text{m}$   
 $Ra = 15.22 \pm 1.12 \mu\text{m}$      $Ra = 17.90 \pm 1.18 \mu\text{m}$

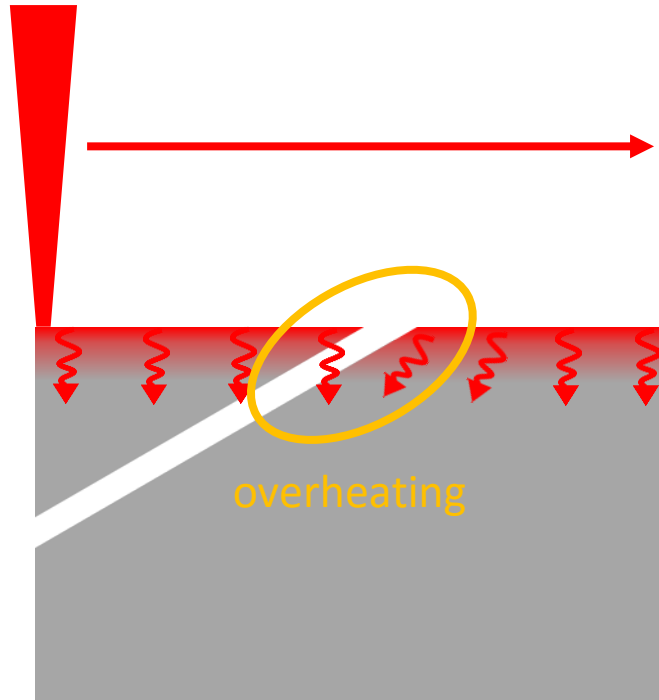


60  $\mu\text{m}$   
 $Ra = 18.13 \pm 0.79 \mu\text{m}$      $Ra = 20.06 \pm 1.32 \mu\text{m}$



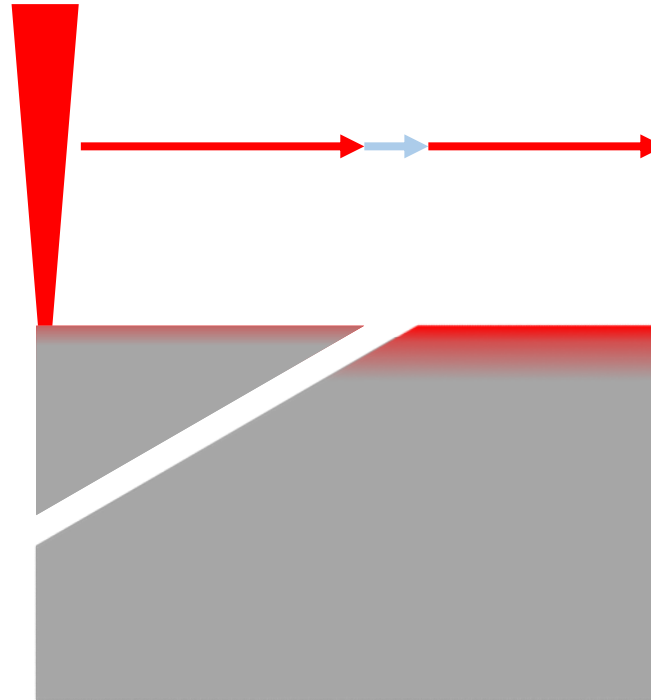
90  $\mu\text{m}$   
 $Ra = 21.99 \pm 1.22 \mu\text{m}$      $Ra = 24.66 \pm 2.03 \mu\text{m}$

# Experimental results: 30° samples



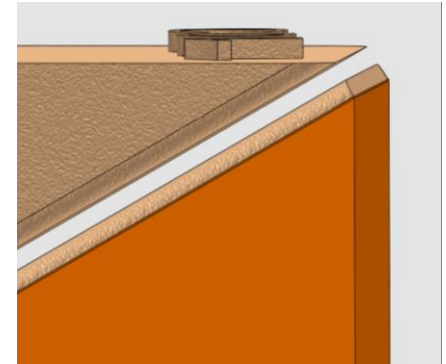
Standard strategy

*[The influence of heat accumulation on the surface roughness in powder-bed additive manufacturing, Mahdi Jamshidinia and Radovan Kovacevic, 2015]*

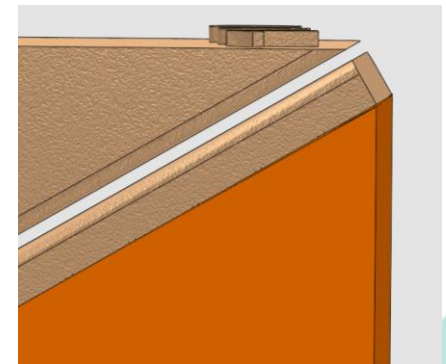


Buffer time between part and support

Support blade thickness



Thin

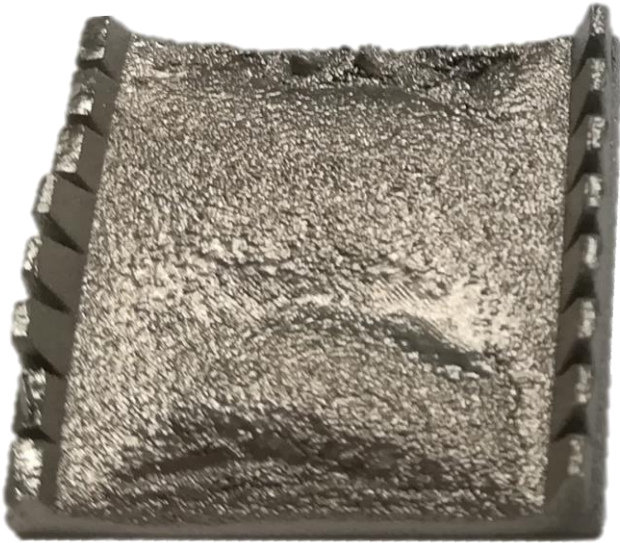


Thick



# Understanding the gap behavior

unsuported

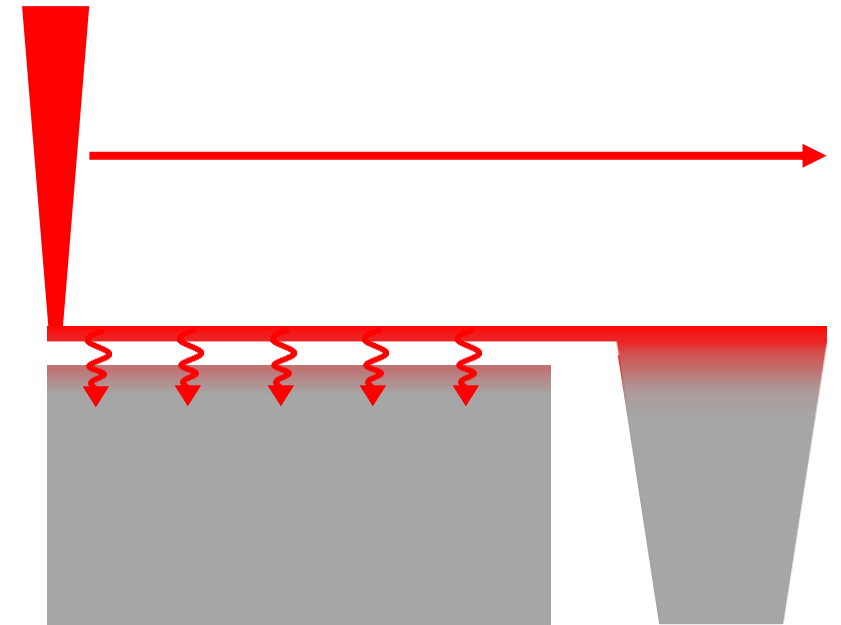


suported

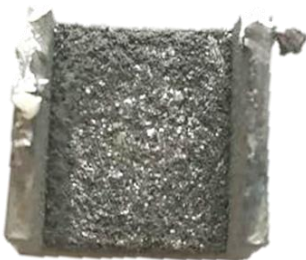


30  $\mu\text{m}$

$R_a = 16.98 \pm 1.54 \mu\text{m}$



$R_a = 19.83 \pm 1.45 \mu\text{m}$



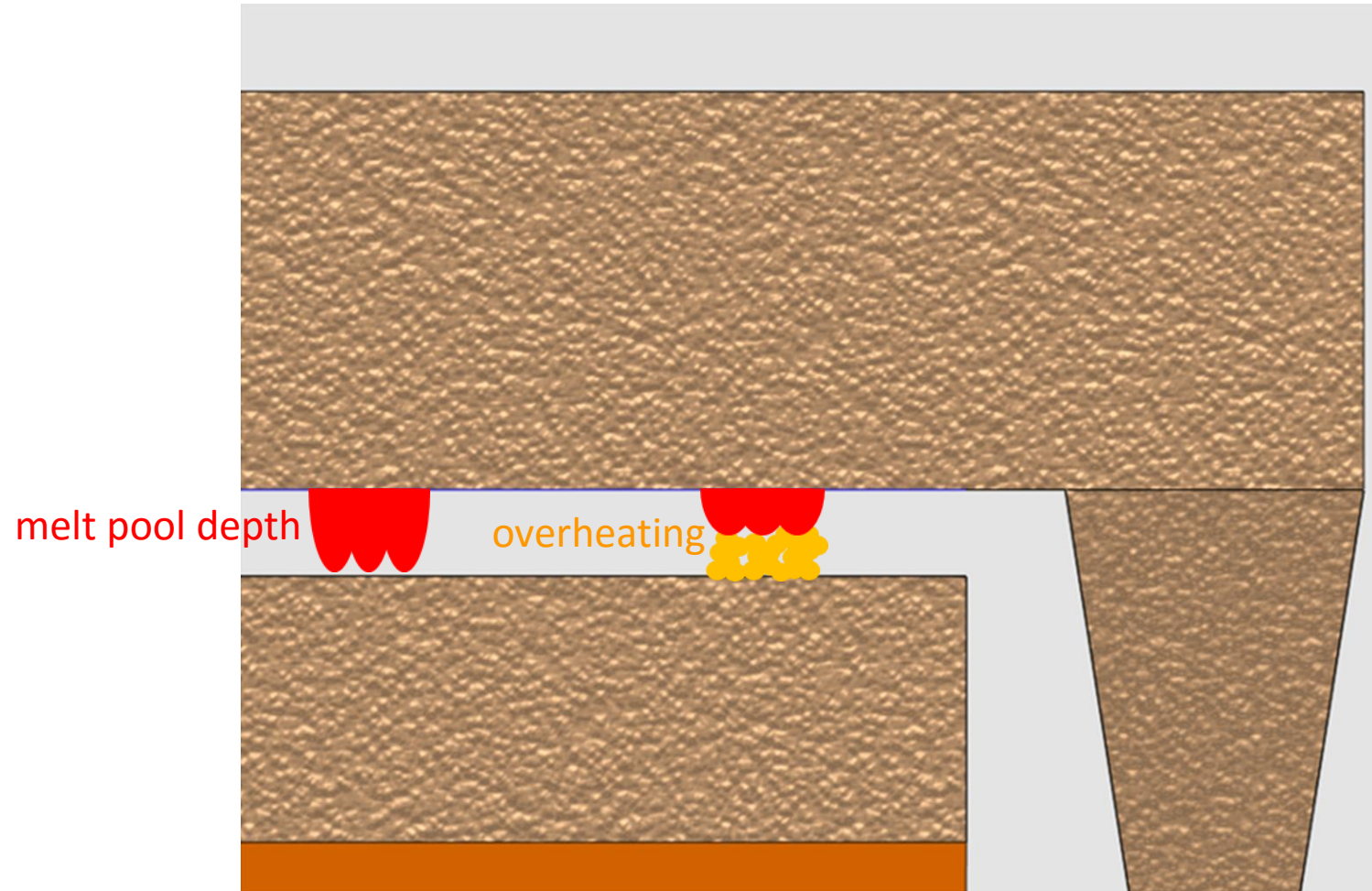
60  $\mu\text{m}$



90  $\mu\text{m}$

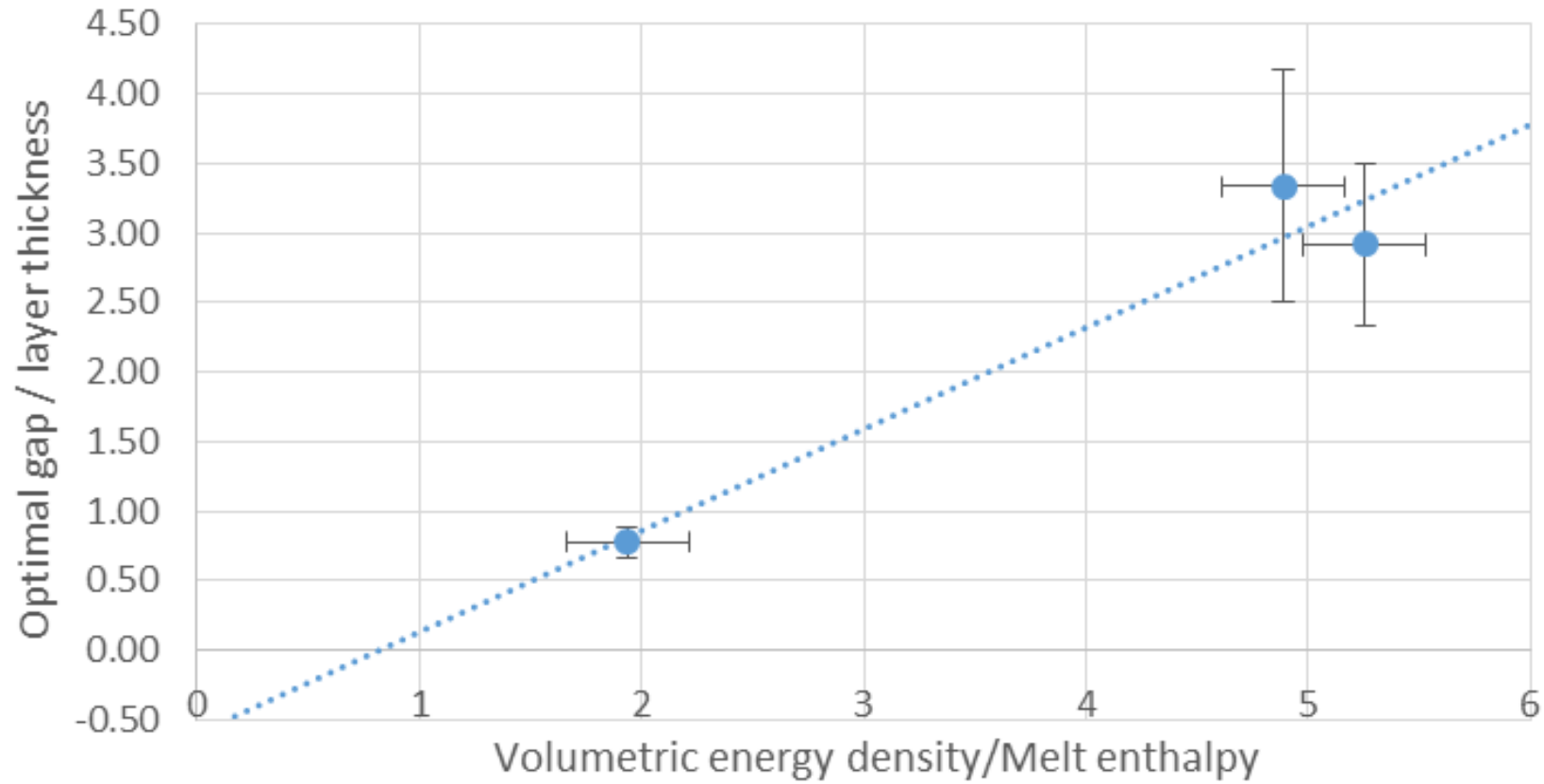
$R_a = 25.02 \pm 2.12 \mu\text{m}$

# Root cause analysis



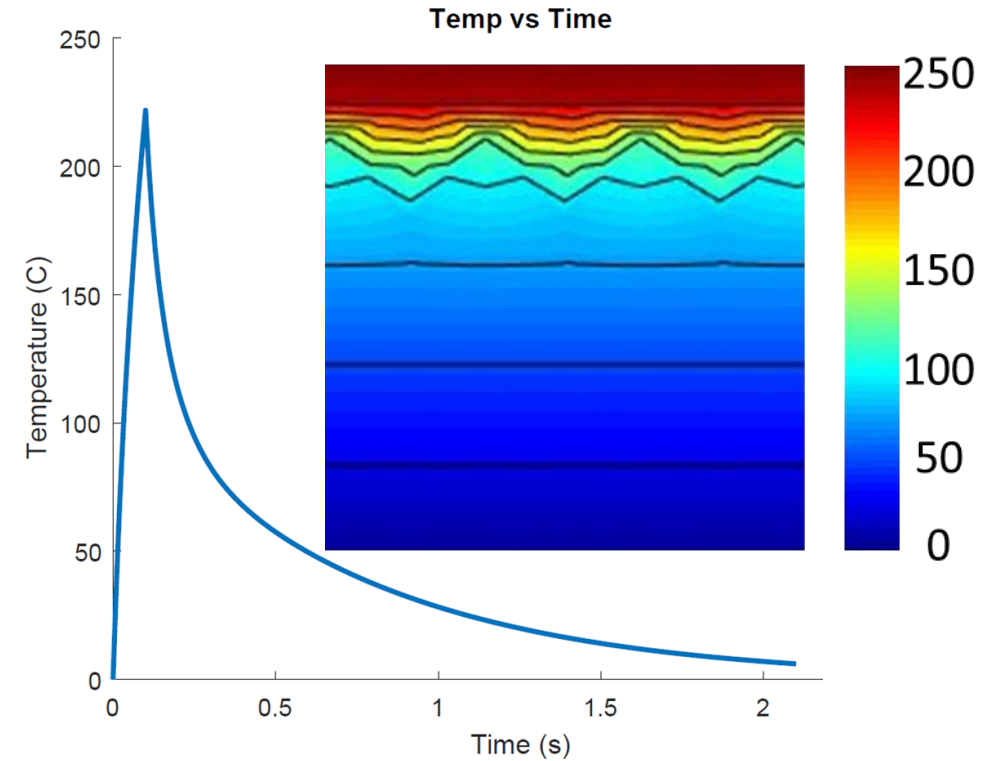
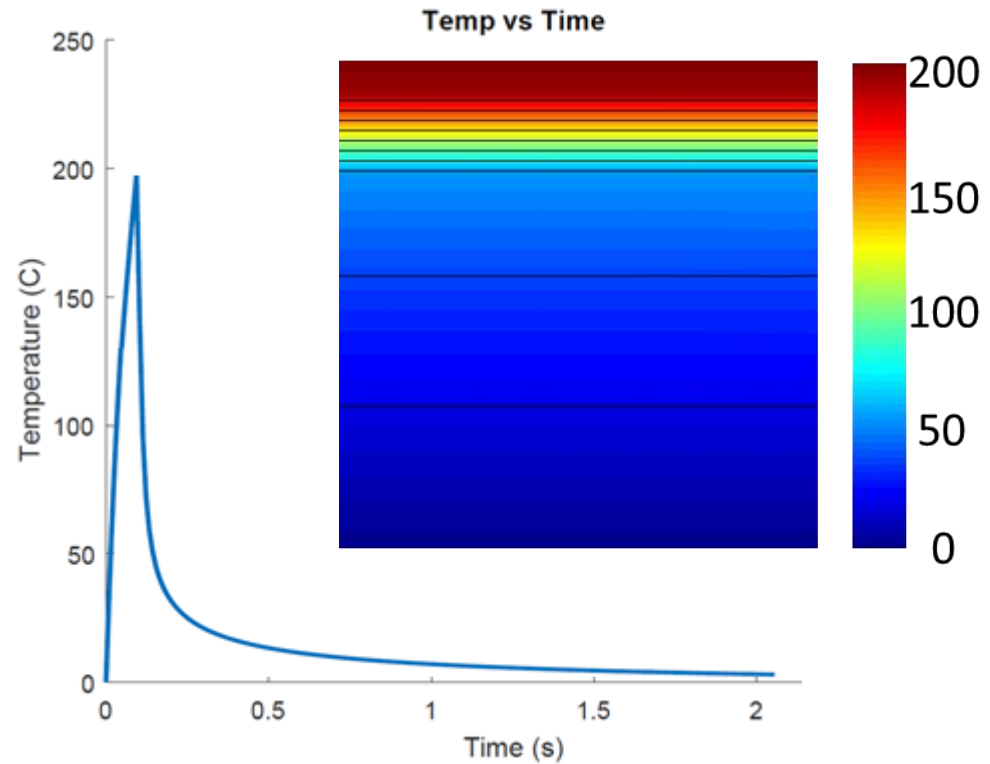
# Root cause analysis

Normalized optimal gap dimension

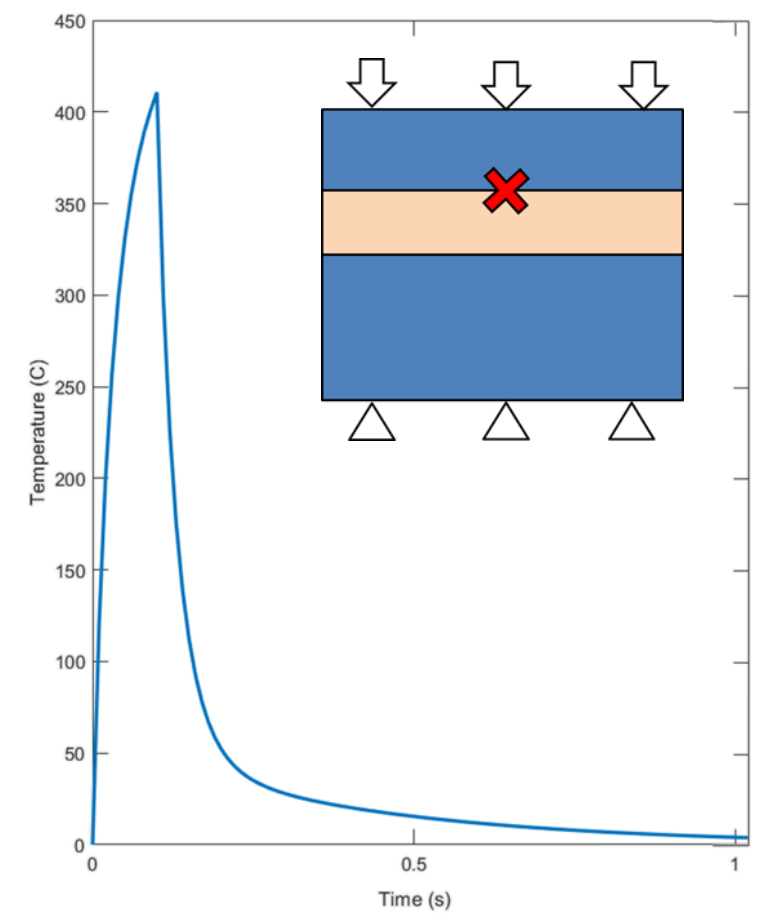
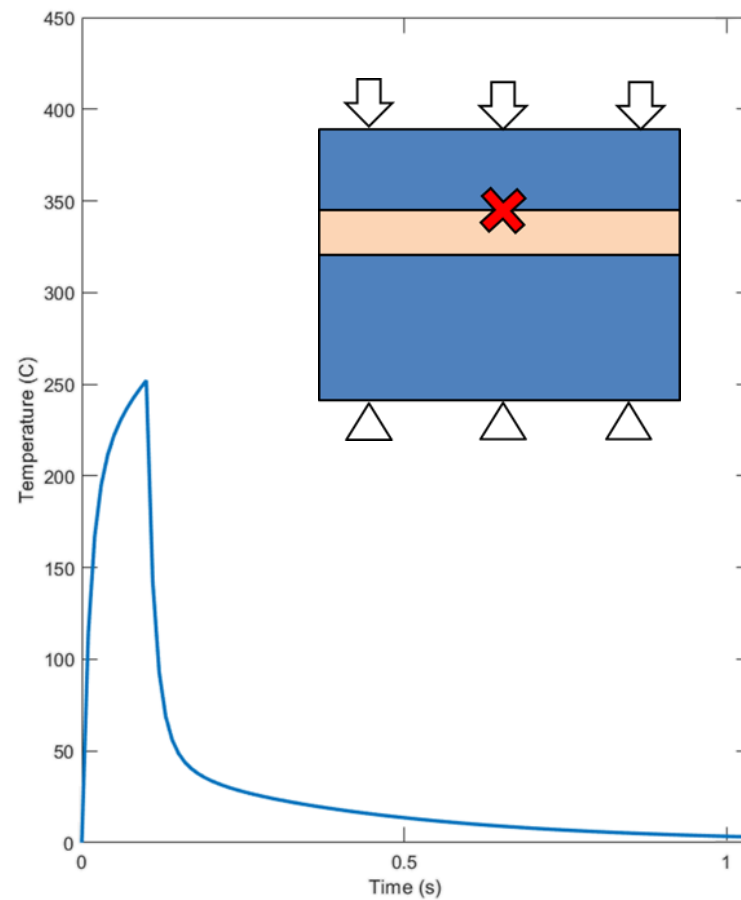
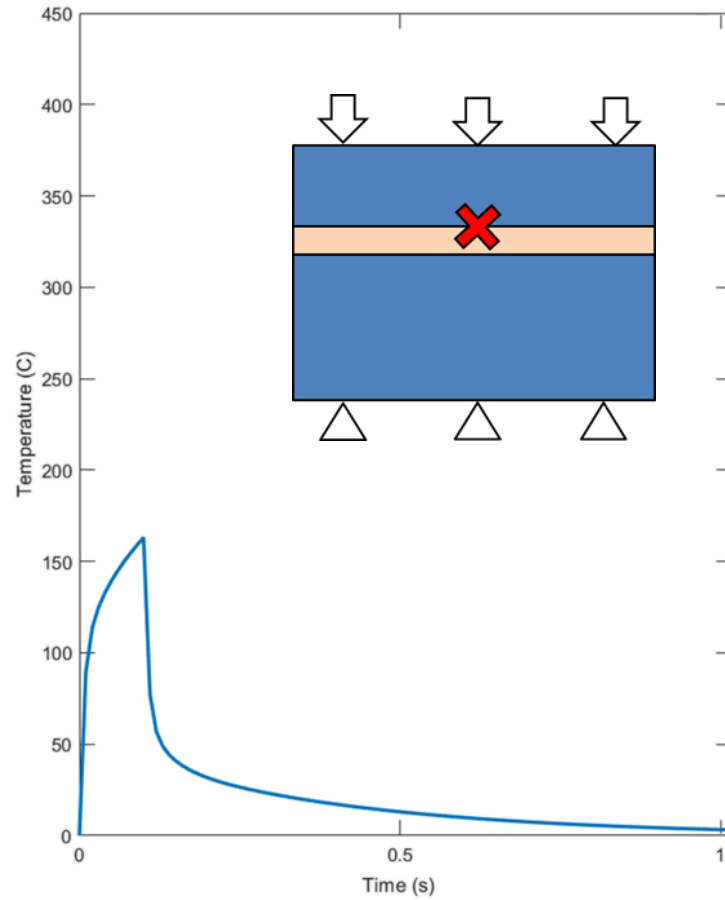




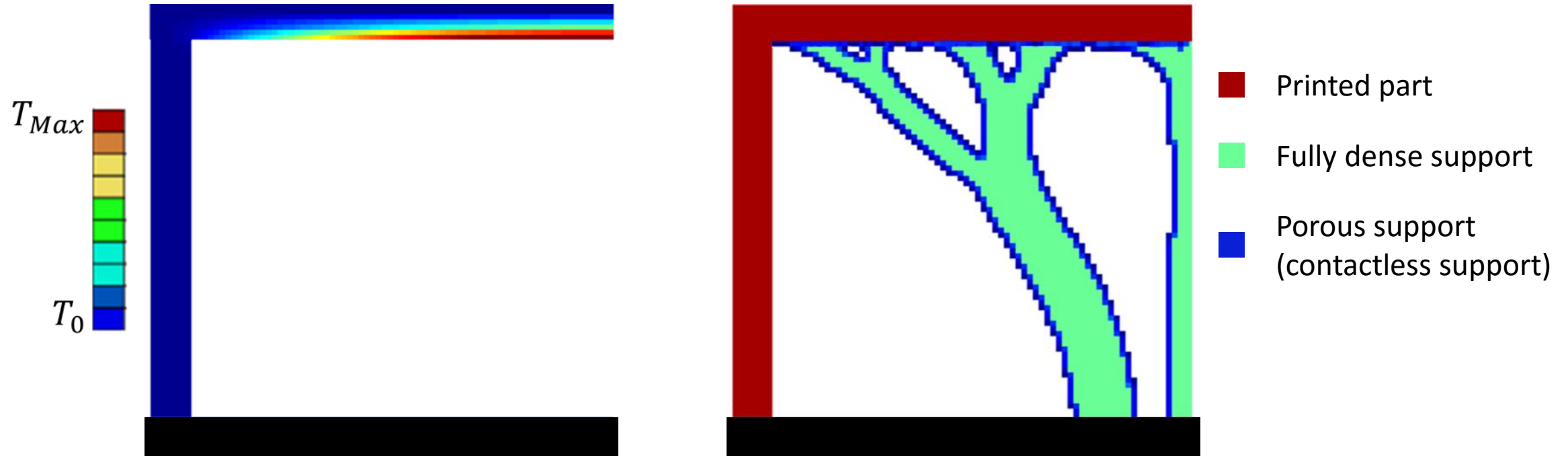
# Thermal simulation



# Thermal simulation



# Thermal simulation



1. On sloped downfacing the powder is overheated by the part and the support which are scanned simultaneously in the same layer. Slightly better results are obtained if a buffer time is applied between the printing of the two regions.
2. On flat overhangs the thermal support (printed several layers before the part) efficiently dissipate the incoming heat. A sensible increase in geometrical accuracy is observed.
3. The thermal simulation suggest that the main feature that defines the optimal gap distance in the flat overhangs is the melt pool depth and not the overheating of the powder in the gap.